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Product Evaluation Report

of

Hardware and Glass Group LLC BR80 Railing System with Monolithic/Laminated Glass

Report No. 8127

Current Florida Building Code

Category: Railings
Sub-Category: Glass Railing

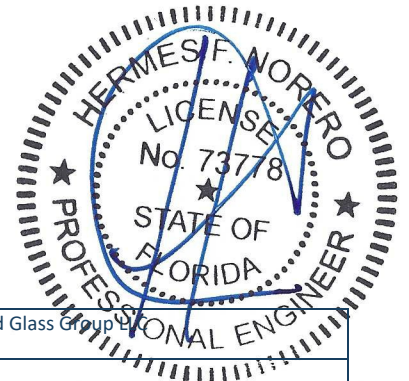
Product: BR80 Railing System with Monolithic/Laminated Glass
Materials: Aluminum 6063-T6

Prepared for:
Hardware and Glass Group LLC
8 The Green Suite #7407
Dover, DE 19901

Prepared by:
Hermes F. Norero, P.E.
Florida Professional Engineer # 73778
Date: 8/3/2022

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Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
		Project #: EEV-22-0712	
	Engineer: LL	PER: 8127	Page #: Page 1 of 60



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Manufacturer: Hardware and Glass Group LLC

Product Name: BR80 Railing System with Monolithic/Laminated Glass

Scope: This is a Product Evaluation Report issued by Hermes F. Norero, P.E. (FL # 73778) for **Hardware and Glass Group LLC**.

Hermes F. Norero, P.E. does not have nor will acquire financial interest in the company manufacturing or distributing the product or in any other entity involved in the approval process of the product named herein.

This product has been evaluated for use in locations adhering to the current Edition of the Florida Building Code.

See Installation Instructions “**BR80-T3680**”, signed and sealed by Hermes F. Norero, P.E. (FL # 73778) for specific use parameters.

Limits of Use:

1. This product has been evaluated and is in compliance with the current Edition of the Florida Building Code, excluding the “High Velocity Hurricane Zone” (HVHZ).
2. Product anchors shall be as listed and spaced as shown on details. Anchor embedment into concrete substrate (Min. F’c = Refer to Appendix).
3. When used in areas requiring wind borne debris protection this product complies with Chapter 16 of the current Edition of the Florida Building Code and does require an impact resistant covering in areas requiring Impact Resistance.
4. Site conditions that deviate from the details of drawing “**BR80-T3680**”, require further engineering analysis by a licensed engineer or registered architect.
5. See Installation Instructions “**BR80-T3680**”, for size and design pressure limitations.

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Performance Standards: The product described herein has been tested per:

- TAS 202-94 (ASTM E330)
- Concentrated and Distributed Load per the current Florida Building Code, Section 1618.4.6
- ANSI Z97.1

Referenced Data:

1. Product Testing performed by **Blackwater Testing Inc.**
(FBC Organization # TST10394)
Report #: BT-HWG-19-001 Report Date: 12/06/2019
Signed and sealed by Constantin Bortes, FL PE #77915

Installation:

Refer to Installation Instructions (“**BR80-T3680**”) for more details of the installation details.

Design Pressure:

Refer to Installation Instructions (“**BR80-T3680**”) for design pressures dependent on reinforcements, hardware type, configuration, and size of units.

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APPENDIX

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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13/16” Laminated Glass (Tested)

Glass Calculations

Wind Load Tables

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WIND LOAD ANALYSIS

To not exceed the maximum stress and deflection of the glass from the analysis, the glass has been analyzed under the following cases for sizes different than tested, but within the square footage of the testing.

• **Live Load:**

- **50 lb/ft distributed load:** The distributed load has been considered for the stress and deflection limitations for the glass.

- Stress: The allowable glass stress is 6000 psi (24000 psi with a safety factor of 4).

$$H_{D.L.O.} = \frac{12 * \theta * [1/6 * ta^2]}{50 \text{ lb/ft}}$$

- Deflection: 1" max.

$$Deflection = \frac{50 \text{ lb} * H_{D.L.O.}^3}{3 * 10.4 * 10^6 \text{ psi} * b * ta^3}$$

$$H_{D.L.O.} = \sqrt[3]{\frac{3 * 10.4 * 10^6 \text{ psi} * b * ta^3 * Deflection}{50 \text{ lb}}}$$

$H_{D.L.O.}$ = Unsupported glass height, in.
 b = Glass pane width, in.
 $Deflection$ = 1 in.
 θ = Allowable Glass Stress, psi.
 ta = Effective Glass Thickness, in.

- **Concentrated Load:** The concentrated load has been considered for the stress and deflection limitations using the following values:

- Stress: The allowable glass stress is 6000 psi (24000 psi with a safety factor of 4).

$$H_{D.L.O.} = \frac{12 * \theta * [\frac{1}{6} * b * ta^2]}{200 \text{ lb}}$$

- Deflection: 1" max.

$$Deflection = \frac{200 \text{ lb} * H_{D.L.O.}^3 * [1 + b/(H_{D.L.O.}/2)]^{1/2}}{3 * 10.4 * 10^6 \text{ psi} * b * ta^3}$$

$H_{D.L.O.}$ = Unsupported glass height, in.
 b = Glass pane width, in.
 $Deflection$ = 1 in.
 θ = Allowable Glass Stress, psi.
 ta = Effective Glass Thickness, in.

*The concentrated load maximum D.L.O. Height was obtained using iterations.

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• **Wind Load:**

- **Design Pressure:** The design pressure proposed for different glass dimensions is based on the equivalent pressure require to produce the same moment at the base of unsupported glass (top of base shoe). Deflection measurements were also simulated using Kuraray Co., Ltd.'s Glass Calculator and Window Glass Design 5 by Standards Design Group, Inc. Deflections were limited to H/24 + L/96 or H/12, whichever lower, according to ASTM E2358 requirements.

$$M_0 = M_x$$

$$M_0 = \frac{DP_x * H_{D.L.O.}^2}{2 * 144}$$

$$DP_x = \frac{2 * 144 * M_0}{H_{D.L.O.}^2}$$

M_0 = Moment from testing, lb-in/in.
 $H_{D.L.O.}$ = Unsupported glass height, in.
 DP_x = Design Pressure for a specific glass D.L.O. Height, psf.

Test Report Data

Glass:	
Glass pane width:	48.03 in
Unsupported Glass Pane Height	39.81 in
Design Pressure	50.00 psf
Single Lite Thickness	0.38 in
Interlayer Thickness	0.09 in
Glass Section Modulus	0.02 in ³ /in
Area of Glass Tested:	13.28 ft ²
Tested Moment at base of unsupported glass:	275.15 lb-in/in
Glass Stress	24000 psi
Safety Factor	4
Allowable Glass Stress	6000 psi
Max. Deflection:	
ICC AC 439 (200 lbs Conc. Load & 50 plf Dist. Load)	1 in
ASTM E2358 (h/24 + l/96 or h/12, Wind Loads)	2.16 in

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Deflection values were limited based on the required measurements below,

Max Deflection per H/24 + L/96 (in)							
		D.L.O Height					
		36	39.81	42	48	60	72
D.L.O Width	12	1.63	1.78	1.88	2.13	2.63	3.13
	24	1.75	1.91	2.00	2.25	2.75	3.25
	36	1.88	2.03	2.13	2.38	2.88	3.38
	48	2.00	2.16	2.25	2.50	3.00	3.50
	60	2.13	2.28	2.38	2.63	3.13	3.63
	72	2.25	2.41	2.50	2.75	3.25	3.75

Max Deflection per H/12 (in)							
		Railing Height					
		40	44	46	52	64	76
Railing Width	12	3.33	3.67	3.83	4.33	5.33	6.33
	24	3.33	3.67	3.83	4.33	5.33	6.33
	36	3.33	3.67	3.83	4.33	5.33	6.33
	48	3.33	3.67	3.83	4.33	5.33	6.33
	60	3.33	3.67	3.83	4.33	5.33	6.33
	72	3.33	3.67	3.83	4.33	5.33	6.33

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Results

Concentrated Load Height Iterations (Fall Protection Requirements Only)

Glass Width		12
Height	Deflection	Target Deflection
50	0.91	1.00
52.29	1.03	
51.56	0.99	
51.79	1.00	
51.72	1.00	
51.74	1.00	
51.73	1.00	
51.74	1.00	
51.73	1.00	
51.74	1.00	
51.74	1.00	
51.74	1.00	
51.74	1.00	
51.74	1.00	
51.74	1.00	
51.74	1.00	

Glass Width		24
Height	Deflection	Target Deflection
50.00	0.35	1.00
84.23	1.36	
72.17	0.91	
75.63	1.03	
74.58	0.99	
74.89	1.00	
74.80	1.00	
74.83	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	
74.82	1.00	

Glass Width		36
Height	Deflection	Target Deflection
50.00	0.21	1.00
109.33	1.57	
87.34	0.88	
93.34	1.04	
91.54	0.99	
92.07	1.00	
91.91	1.00	
91.96	1.00	
91.94	1.00	
91.95	1.00	
91.95	1.00	
91.95	1.00	
91.95	1.00	
91.95	1.00	
91.95	1.00	
91.95	1.00	

Glass Width		48
Height	Deflection	Target Deflection
100	0.90	1.00
105.44	1.03	
103.85	0.99	
104.31	1.00	
104.17	1.00	
104.21	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	
104.20	1.00	

Glass Width		60
Height	Deflection	Target Deflection
100.00	0.73	1.00
117.38	1.09	
112.18	0.97	
113.64	1.01	
113.22	1.00	
113.34	1.00	
113.31	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	
113.32	1.00	

Glass Width		72
Height	Deflection	Target Deflection
110.00	0.79	1.00
123.52	1.07	
119.58	0.98	
120.68	1.01	
120.37	1.00	
120.45	1.00	
120.43	1.00	
120.44	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	
120.43	1.00	

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GLASS PANE WIDTH (IN)	EFFECTIVE GLASS THICKNESS		MOMENT AT TOP OF BASE SHOE (LB-IN/IN)	ALLOWABLE DESIGN PRESSURE (PSF)						200 LB LIVE LOAD		50 LB/FT LIVE LOAD	
	DEFLECTION (IN)	STRESS (IN)		UNSUPPORTED GLASS HEIGHT (IN)						MAX. UNSUPPORTED GLASS HEIGHT (IN)		MAX. UNSUPPORTED GLASS HEIGHT (IN)	
				36	39.81	42	48	60	72	STRESS	DEFLECTION	STRESS	DEFLECTION
12	0.5240	0.5907	275.1	61.1	50.0	44.9	34.4	22.0	15.3	20.9	51.7	83.7	44.8
24	0.6269	0.6880	275.1	61.1	50.0	44.9	34.4	22.0	15.3	56.8	74.8	113.6	53.6
36	0.6913	0.7365	275.1	61.1	50.0	44.9	34.4	22.0	15.3	97.6	91.9	130.2	59.1
48	0.7281	0.7603	275.1	61.1	50.0	44.9	34.4	22.0	15.3	138.7	104.2	138.7	62.2
60	0.7498	0.7731	275.1	61.1	50.0	44.9	34.4	22.0	15.3	179.3	113.3	143.4	64.1
72	0.7633	0.7806	275.1	61.1	50.0	44.9	34.4	22.0	15.3	219.4	120.4	146.3	65.2

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1/2" Monolithic Glass

Glass Calculations

Wind Load Tables

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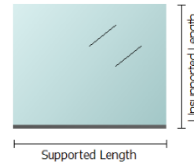


Input

July 21, 2022

Glazing Information

Supported Edges: One side Supported
 Shape: Rectangular
 Unsupported Length: 39.0 in.
 Supported Length: 48.0 in.
 Glazing Angle: 90.0 °



Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
 Heat Treatment: Fully Tempered

Applied Loads

Description	Load	Duration
Short Duration	50.0 psf	3.00 sec

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ASTM E1300 Ext. Basic (8/1000)
Load Resistance Report

July 21, 2022

Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
Heat Treatment: Fully Tempered

Load Resistance

Short Duration (3 Sec)

Description	NFL	GTF	LR
Single Lite	16.7 psf	4.00	66.6 psf

Comparisons

Scenario - Short Duration
 50.0 psf 3.00 sec <= 66.6 psf OK
 Approximate edge of glass deflection
 Single Lite 1.21 in.

Notes

Load resistance values are computed in accordance with ASTM E1300-16 Section 6.2 and are based on non-factored load values calculated in a manner consistent with those presented in ASTM E1300-16.

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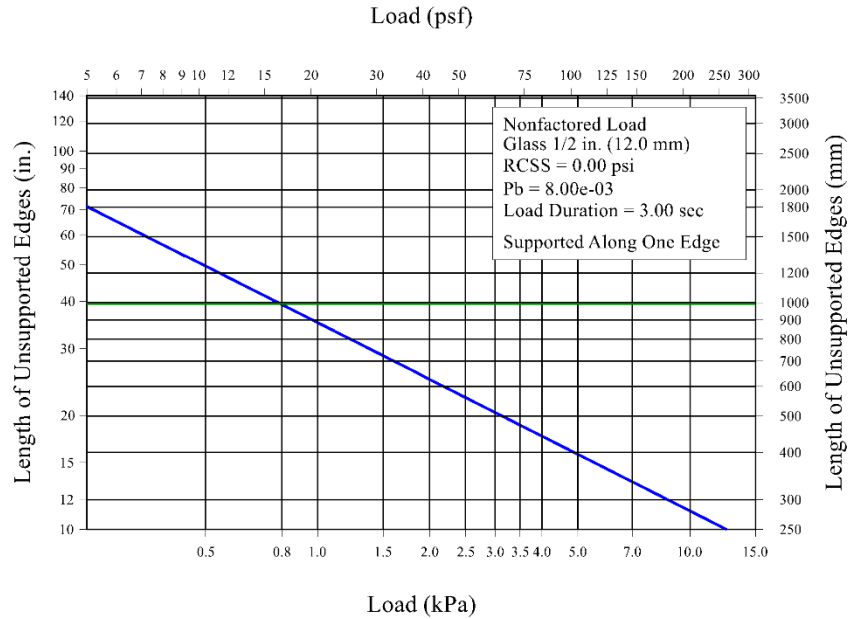


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ASTM E1300 Ext. Basic (8/1000)
 Load Resistance Details

July 21, 2022



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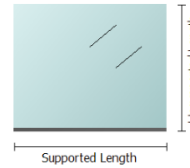
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Input

July 29, 2022

Glazing Information

Supported Edges: One side Supported
 Shape: Rectangular
 Unsupported Length: 60.0 in.
 Supported Length: 72.0 in.
 Glazing Angle: 90.0 °



Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
 Heat Treatment: Fully Tempered

Applied Loads

Description	Load	Duration
Short Duration	19.4 psf	3.00 sec

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ASTM E1300 Ext. Basic (8/1000)
Load Resistance Report

July 29, 2022

Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
Heat Treatment: Fully Tempered

Load Resistance

Short Duration (3 Sec)

Description	NFL	GTF	LR
Single Lite	7.0 psf	4.00	28.2 psf

Comparisons

Scenario - Short Duration
19.4 psf 3.00 sec <= 28.2 psf
Approximate edge of glass deflection
Single Lite

OK

2.62 in.

Notes

Load resistance values are computed in accordance with ASTM E1300-16 Section 6.2 and are based on non-factored load values calculated in a manner consistent with those presented in ASTM E1300-16.

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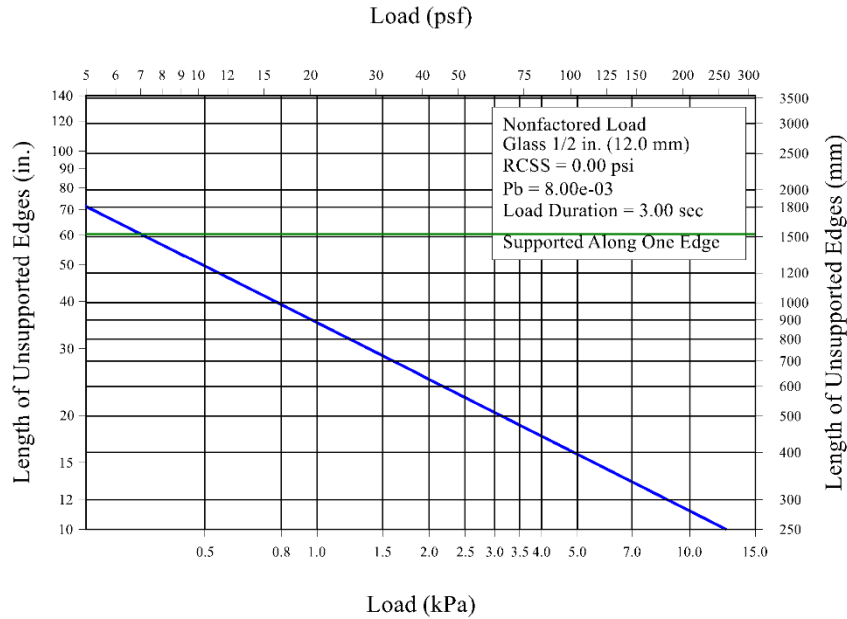


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ASTM E1300 Ext. Basic (8/1000)
 Load Resistance Details

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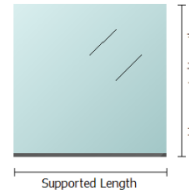


Input

July 29, 2022

Glazing Information

Supported Edges: One side Supported
 Shape: Rectangular
 Unsupported Length: 72.0 in.
 Supported Length: 72.0 in.
 Glazing Angle: 90.0 °



Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
 Heat Treatment: Fully Tempered

Applied Loads

Description	Load	Duration
Short Duration	11.1 psf	3.00 sec

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ASTM E1300 Ext. Basic (8/1000)
Load Resistance Report

July 29, 2022

Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 1/2 in.
Heat Treatment: Fully Tempered

Load Resistance

Short Duration (3 Sec)

Description	NFL	GTF	LR
Single Lite	4.9 psf	4.00	19.6 psf

Comparisons

Scenario - Short Duration
11.1 psf 3.00 sec <= 19.6 psf
Approximate edge of glass deflection
Single Lite

OK

3.11 in.

Notes

Load resistance values are computed in accordance with ASTM E1300-16 Section 6.2 and are based on non-factored load values calculated in a manner consistent with those presented in ASTM E1300-16.

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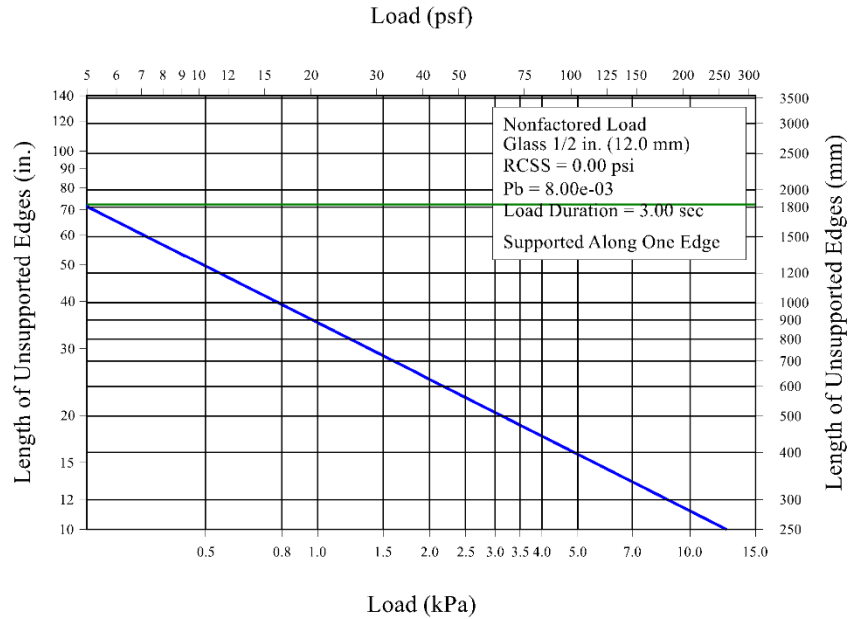


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ASTM E1300 Ext. Basic (8/1000)
 Load Resistance Details

July 29, 2022



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9/16” Laminated Glass

Glass Calculations

Wind Load Tables

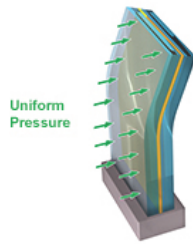
Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
		Project #: EEV-22-0712	
	Engineer: LL	PER: 8127	Page #: Page 23 of 60

Your calculated results

SIDE SUPPORTED BEAM

PROJECT TITLE:

FIRM NAME: Hardware and Glass



Calculation according to ASTM E1300
 Results do not include gravity

*= Field requires no data input by user

Case 3: Uniform Pressure (psi)

INPUTS

Glass Span: (in)
 Uniform Load: (psi)

GLASS PROPERTIES:

Type of Glass:
 Nominal Single Glass Thickness:
 Minimum Single Glass Thickness*: (in)
 Allowable Stress*: (psi)

INTERLAYER:

Thickness: (in)

INTERLAYER PROPERTIES:

Load Duration:
 Temperature:

RESULTS

Material	Shear Modulus	Youngs Modulus
SentryGlas®	27985 psi	81345 psi
Standard PVB	140.8 psi	422.3 psi
 Sifol® EXTRA STIFF	8412.19 psi	24511.4 psi

» Your calculated results:

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Effective Thickness for Glass Stress	SentryGlas®:	0.497 in
	Trosifol® EXTRA STIFF	0.494 in
	Standard PVB:	0.401 in
Effective Thickness for Laminate Deflection	SentryGlas®:	0.496 in
	Trosifol® EXTRA STIFF	0.491 in
	Standard PVB:	0.359 in
Glass Stress ✓ Meets ASTM E1300 ✗ Fails ASTM E1300	SentryGlas®:	✓ 6423.052 psi
	Trosifol® EXTRA STIFF	✓ 6482.977 psi
	Standard PVB:	✓ 9861.461 psi
Laminate Deflection	SentryGlas®:	0.951 in
	Trosifol® EXTRA STIFF	0.979 in
	Standard PVB:	2.507 in
Calculation according to ASTM E1300		

 PRINT RESULTS

 DOWNLOAD RESULTS

 NEW CALCULATION

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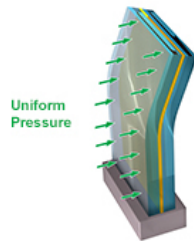
Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Your calculated results

SIDE SUPPORTED BEAM

PROJECT TITLE:

FIRM NAME: Hardware and Glass



Calculation according to ASTM E1300
 Results do not include gravity

*= Field requires no data input by user

Case 3: Uniform Pressure (psi)

INPUT DATA

Glass Span: (in)
 Uniform Load: (psi)

GLASS PROPERTIES:

Type of Glass: ▼
 Nominal Single Glass Thickness: ▼
 Minimum Single Glass Thickness*: (in)
 Allowable Stress*: (psi)


INTERLAYER:

Thickness: ▼ (in)

INTERLAYER PROPERTIES:

Load Duration: ▼
 Temperature: ▼

RESULTS

Material	Shear Modulus	Youngs Modulus
SentryGlas®	27985 psi	81345 psi
Standard PVB	140.8 psi	422.3 psi
 sifol® EXTRA STIFF	8412.19 psi	24511.4 psi

» Your calculated results:

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Effective Thickness for Glass Stress	SentryGlas®:	0.497 in
	Trosifol® EXTRA STIFF	0.497 in
	Standard PVB:	0.452 in
Effective Thickness for Laminate Deflection	SentryGlas®:	0.497 in
	Trosifol® EXTRA STIFF	0.496 in
	Standard PVB:	0.422 in
Glass Stress ✓ Meets ASTM E1300 ✗ Fails ASTM E1300	SentryGlas®:	✓ 6225.647 psi
	Trosifol® EXTRA STIFF	✓ 6243.211 psi
	Standard PVB:	✓ 7522.743 psi
Laminate Deflection	SentryGlas®:	3.124 in
	Trosifol® EXTRA STIFF	3.151 in
	Standard PVB:	5.125 in
Calculation according to ASTM E1300		

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Glass Composition

Glass:		
Glass pane width:	48.03	in
Unsupported Glass Pane Height	39.81	in
Design Pressure	50.00	psf
Single Lite Thickness	0.25	in
Interlayer Thickness	0.06	in
Glass Section Modulus	0.01	in ³ /in
Area of Glass Tested:	13.28	ft ²
Tested Moment at base of unsupported glass:	275.15	lb-in/in
Glass Stress	24000	psi
Safety Factor	4	
Allowable Glass Stress	6000	psi
Max. Deflection		
ICC AC 439 (200 lbs Conc. Load & 50 plf Dist. Load)	1	in
ASTM E2358 (h/24 + l/96 or h/12, Wind Loads)	2.16	in

Results

Concentrated Load Height Iterations (Fall Protection Requirements Only)

Glass Width		12
Height	Deflection	Target Deflection
50	2.74	1.00
30.23	0.74	
35.22	1.09	
33.66	0.97	
34.12	1.01	
33.98	1.00	
34.02	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	
34.01	1.00	

Glass Width		24
Height	Deflection	Target Deflection
50.00	1.07	1.00
48.41	0.98	
48.86	1.01	
48.73	1.00	
48.77	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	
48.76	1.00	

Glass Width		36
Height	Deflection	Target Deflection
50.00	0.70	1
59.90	1.11	
56.96	0.97	
57.77	1.01	
57.54	1.00	
57.61	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	
57.59	1.00	

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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11/16” Laminated Glass

Glass Calculations

Wind Load Tables

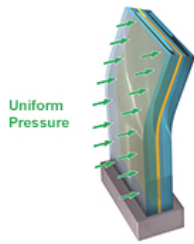
Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Your calculated results

SIDE SUPPORTED BEAM

PROJECT TITLE:

FIRM NAME: Hardware and Glass



Calculation according to ASTM E1300
 Results do not include gravity

*= Field requires no data input by user

Case 3: Uniform Pressure (psi)

Glass Span: (in)
 Uniform Load: (psi)

GLASS PROPERTIES:

Type of Glass: ▼
 Nominal Single Glass Thickness: ▼
 Minimum Single Glass Thickness*: (in)
 Allowable Stress*: (psi)

INTERLAYER:

Thickness: ▼ (in)

INTERLAYER PROPERTIES:

Load Duration: ▼
 Temperature: ▼

Material	Shear Modulus	Youngs Modulus
SentryGlas®	27985 psi	81345 psi
Standard PVB	140.8 psi	422.3 psi
 Sifol® EXTRA STIFF	8412.19 psi	24511.4 psi

» Your calculated results:

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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	Engineer: LL	PER: 8127	Page #: Page 31 of 60

Effective Thickness for Glass Stress	SentryGlas®:	0.642 in
	Trosifol® EXTRA STIFF	0.638 in
	Standard PVB:	0.506 in
Effective Thickness for Laminate Deflection	SentryGlas®:	0.64 in
	Trosifol® EXTRA STIFF	0.632 in
	Standard PVB:	0.452 in
Glass Stress ✓ Meets ASTM E1300 ✗ Fails ASTM E1300	SentryGlas®:	✓ 3841.58 psi
	Trosifol® EXTRA STIFF	✓ 3889.901 psi
	Standard PVB:	✓ 6186.579 psi
Laminate Deflection	SentryGlas®:	0.441 in
	Trosifol® EXTRA STIFF	0.458 in
	Standard PVB:	1.252 in

Calculation according to ASTM E1300

 PRINT RESULTS

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Glass Composition

Glass:		
Glass pane width:	48.03	in
Unsupported Glass Pane Height	39.81	in
Design Pressure	50.00	psf
Single Lite Thickness	0.31	in
Interlayer Thickness	0.06	in
Glass Section Modulus	0.02	in ³ /in
Area of Glass Tested:	13.28	ft ²
Tested Moment at base of unsupported glass:	275.15	lb-in/in
Glass Stress	24000	psi
Safety Factor	4	
Allowable Glass Stress	6000	psi
Max. Deflection		
ICC AC 439 (200 lbs Conc. Load & 50 plf Dist. Load)	1	in
ASTM E2358 (h/24 + l/96 or h/12, Wind Loads)	2.16	in

Results

Concentrated Load Height Iterations (Fall Protection Requirements Only)

Glass Width		12
Height	Deflection	Target Deflection
50	1.37	1.00
42.71	0.91	
44.85	1.03	
44.18	0.99	
44.38	1.00	
44.32	1.00	
44.34	1.00	
44.33	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	
44.34	1.00	

Glass Width		24
Height	Deflection	Target Deflection
50.00	0.53	1.00
68.41	1.20	
62.42	0.95	
64.14	1.02	
63.63	1.00	
63.78	1.00	
63.73	1.00	
63.75	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	
63.74	1.00	

Glass Width		36
Height	Deflection	Target Deflection
50.00	0.34	1
85.82	1.36	
73.65	0.92	
76.97	1.03	
76.00	0.99	
76.28	1.00	
76.20	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	
76.22	1.00	

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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3/4" Monolithic Glass

Glass Calculations

Wind Load Tables

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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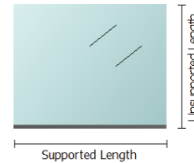


Input

July 21, 2022

Glazing Information

Supported Edges: One side Supported
 Shape: Rectangular
 Unsupported Length: 39.0 in.
 Supported Length: 48.0 in.
 Glazing Angle: 90.0 °



Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 3/4 in.
 Heat Treatment: Fully Tempered

Applied Loads

Description	Load	Duration
Short Duration	50.0 psf	3.00 sec

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022		Customer: Hardware and Glass Group LLC	
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ASTM E1300 Ext. Basic (8/1000)
Load Resistance Report

July 21, 2022

Glazing Construction (Single Glazed Lite)

Single Lite Properties (Monolithic)

Thickness: 3/4 in.
Heat Treatment: Fully Tempered

Load Resistance

Short Duration (3 Sec)

Description	NFL	GTF	LR
Single Lite	39.1 psf	4.00	157 psf

Comparisons

Scenario - Short Duration	
50.0 psf 3.00 sec <= 157 psf	OK
Approximate edge of glass deflection	
Single Lite	0.33 in.

Notes

Load resistance values are computed in accordance with ASTM E1300-16 Section 6.2 and are based on non-factored load values calculated in a manner consistent with those presented in ASTM E1300-16.

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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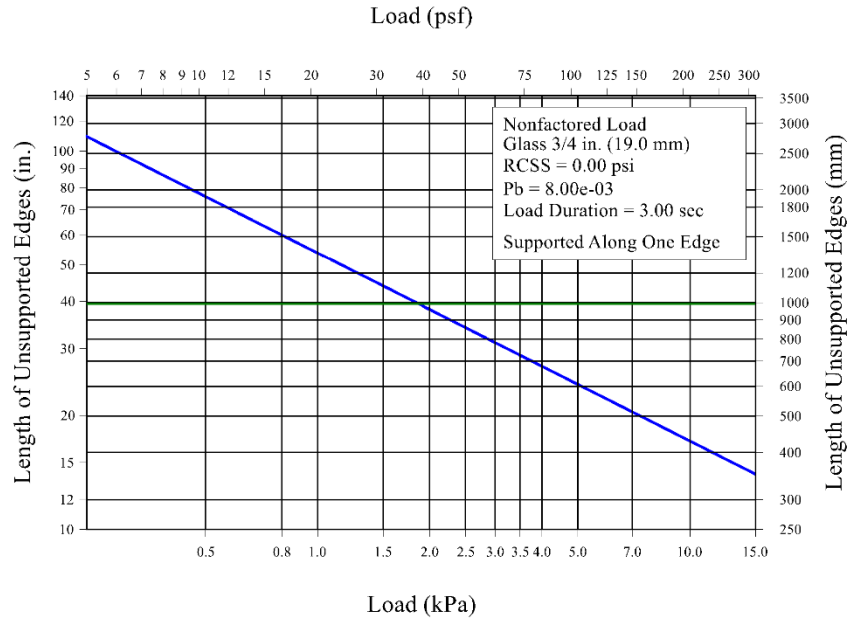


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ASTM E1300 Ext. Basic (8/1000)
 Load Resistance Details

July 21, 2022



Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Glass Composition

Glass:		
Glass pane width:	48.03	in
Unsupported Glass Pane Height	39.81	in
Design Pressure	50.00	psf
Single Lite Thickness	0.75	in
Interlayer Thickness	N/A	
Glass Section Modulus	0.09	in ³ /in
Area of Glass Tested:	13.28	ft ²
Tested Moment at base of unsupported glass:	275.15	lb-in/in
Glass Stress	24000	psi
Safety Factor	4	
Allowable Glass Stress	6000	psi
Max. Deflection		
ICC AC 439 (200 lbs Conc. Load & 50 plf Dist. Load)	1	in
ASTM E2358 (h/24 + l/96 or h/12, Wind Loads)	2.16	in

Results

Concentrated Load Height Iterations (Fall Protection Requirements Only)

Glass Width		12
Height	Deflection	Target Deflection
50	0.35	1.00
84.05	1.41	
70.89	0.89	
75.08	1.04	
73.66	0.99	
74.13	1.00	
73.97	1.00	
74.03	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	
74.01	1.00	

Glass Width		24
Height	Deflection	Target Deflection
50.00	0.23	1.00
103.46	1.55	
83.16	0.87	
89.00	1.04	
87.16	0.99	
87.73	1.00	
87.55	1.00	
87.60	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	
87.59	1.00	

Glass Width		36
Height	Deflection	Target Deflection
50.00	0.19	1.00
115.96	1.62	
91.00	0.87	
97.82	1.04	
95.76	0.99	
96.36	1.00	
96.18	1.00	
96.24	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	
96.22	1.00	

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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27/32” Laminated Glass

Glass Calculations

Wind Load Tables

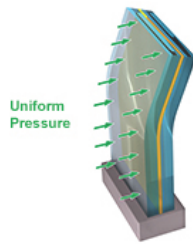
Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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	Engineer: LL	PER: 8127	Page #: Page 41 of 60

Your calculated results

SIDE SUPPORTED BEAM

PROJECT TITLE:

FIRM NAME: Hardware and Glass



Calculation according to ASTM E1300
 Results do not include gravity

*= Field requires no data input by user

Case 3: Uniform Pressure (psi)

Glass Span:	<input type="text" value="39"/>	(in)
Uniform Load:	<input type="text" value="0.347"/>	(psi)

GLASS PROPERTIES:


Type of Glass:	<input type="text" value="Tempered Glass"/>	▼
Nominal Single Glass Thickness:	<input type="text" value="3/8"/>	▼
Minimum Single Glass Thickness*:	<input type="text" value="0.355"/>	(in)
Allowable Stress*:	<input type="text" value="10616.76242"/>	(psi)

INTERLAYER:

Thickness:	<input type="text" value="0.060"/>	▼ (in)
------------	------------------------------------	--------

INTERLAYER PROPERTIES:

Load Duration:	<input type="text" value="3 s"/>	▼
Temperature:	<input type="text" value="75° F"/>	▼

Material	Shear Modulus	Youngs Modulus
SentryGlas®	27985 psi	81345 psi
Standard PVB	140.8 psi	422.3 psi
 Sifol® EXTRA STIFF	8412.19 psi	24511.4 psi

» Your calculated results:

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
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Effective Thickness for Glass Stress	SentryGlas®:	0.767 in
	Trosifol® EXTRA STIFF	0.762 in
	Standard PVB:	0.596 in
Effective Thickness for Laminate Deflection	SentryGlas®:	0.765 in
	Trosifol® EXTRA STIFF	0.754 in
	Standard PVB:	0.533 in
Glass Stress ✓ Meets ASTM E1300 ✗ Fails ASTM E1300	SentryGlas®:	✓ 2689.364 psi
	Trosifol® EXTRA STIFF	✓ 2729.77 psi
	Standard PVB:	✓ 4452.976 psi
Laminate Deflection	SentryGlas®:	0.259 in
	Trosifol® EXTRA STIFF	0.27 in
	Standard PVB:	0.767 in

Calculation according to ASTM E1300

PRINT RESULTS

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NEW CALCULATOR

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1-1/8" Laminated Glass

Glass Calculations

Wind Load Tables

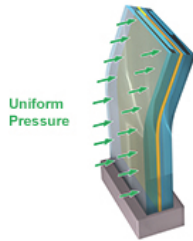
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Your calculated results

SIDE SUPPORTED BEAM

PROJECT TITLE:

FIRM NAME: Hardware and Glass



Calculation according to ASTM E1300
 Results do not include gravity

*= Field requires no data input by user

Case 3: Uniform Pressure (psi)

Input Parameters

Glass Span: (in)
 Uniform Load: (psi)

GLASS PROPERTIES:

Type of Glass:
 Nominal Single Glass Thickness:
 Minimum Single Glass Thickness*: (in)
 Allowable Stress*: (psi)


INTERLAYER:

Thickness: (in)

INTERLAYER PROPERTIES:

Load Duration:
 Temperature:

Material Properties

Material	Shear Modulus	Youngs Modulus
SentryGlas®	27985 psi	81345 psi
Standard PVB	140.8 psi	422.3 psi
 Sifol® EXTRA STIFF	8412.19 psi	24511.4 psi

» Your calculated results:

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Effective Thickness for Glass Stress	SentryGlas®:	0.994 in
	Trosifol® EXTRA STIFF	0.984 in
	Standard PVB:	0.759 in
Effective Thickness for Laminate Deflection	SentryGlas®:	0.989 in
	Trosifol® EXTRA STIFF	0.971 in
	Standard PVB:	0.677 in
Glass Stress ✓ Meets ASTM E1300 ✗ Fails ASTM E1300	SentryGlas®:	✓ 1603.824 psi
	Trosifol® EXTRA STIFF	✓ 1634.939 psi
	Standard PVB:	✓ 2747.78 psi
Laminate Deflection	SentryGlas®:	0.12 in
	Trosifol® EXTRA STIFF	0.126 in
	Standard PVB:	0.373 in

Calculation according to ASTM E1300

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NEW CALCULATION

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Glass Composition

Glass:		
Glass pane width:	48.03	in
Unsupported Glass Pane Height	39.81	in
Design Pressure	50.00	psf
Single Lite Thickness	0.50	in
Interlayer Thickness	0.06	in
Glass Section Modulus	0.04	in ³ /in
Area of Glass Tested:	13.28	ft ²
Tested Moment at base of unsupported glass:	275.15	lb-in/in
Glass Stress	24000	psi
Safety Factor	4	
Allowable Glass Stress	6000	psi
Max. Deflection		
ICC AC 439 (200 lbs Conc. Load & 50 plf Dist. Load)	1	in
ASTM E2358 (h/24 + l/96 or h/12, Wind Loads)	2.16	in

Results

Concentrated Load Height Iterations (Fall Protection Requirements Only)

Glass Width		12
Height	Deflection	Target Deflection
50	0.41	1.00
77.95	1.34	
67.45	0.91	
70.78	1.03	
69.66	0.99	
70.03	1.00	
69.91	1.00	
69.95	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	
69.94	1.00	

Glass Width		24
Height	Deflection	Target Deflection
50.00	0.17	1.00
122.71	1.73	
93.38	0.84	
101.85	1.06	
99.12	0.98	
99.97	1.01	
99.70	1.00	
99.79	1.00	
99.76	1.00	
99.77	1.00	
99.76	1.00	
99.77	1.00	
99.77	1.00	
99.77	1.00	
99.77	1.00	
99.77	1.00	
99.77	1.00	

Glass Width		36
Height	Deflection	Target Deflection
50.00	0.10	1.00
156.88	1.96	
112.12	0.81	
124.38	1.07	
120.52	0.98	
121.68	1.01	
121.33	1.00	
121.44	1.00	
121.40	1.00	
121.41	1.00	
121.41	1.00	
121.41	1.00	
121.41	1.00	
121.41	1.00	
121.41	1.00	
121.41	1.00	

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Anchor Layout Calculations

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Company:		Date:	6/8/2022
Engineer:		Page:	1/6
Project:			
Address:			
Phone:			
E-mail:			

1. Project Information

Customer company:
 Customer contact name:
 Customer e-mail:
 Comment:

Project description:
 Location:
 Fastening description:

2. Input Data & Anchor Parameters

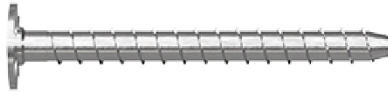
General
 Design method: ACI 318-14
 Units: Imperial units

Anchor Information:
 Anchor type: Concrete screw
 Material: Carbon Steel
 Diameter (inch): 0.500
 Nominal Embedment depth (inch): 4.000
 Effective Embedment depth, h_{ef} (inch): 2.990
 Code report: ICC-ES ESR-2713
 Anchor category: 1
 Anchor ductility: No
 h_{min} (inch): 6.25
 c_{ac} (inch): 4.50
 c_{min} (inch): 1.75
 s_{min} (inch): 3.00

Base Material
 Concrete: Normal-weight
 Concrete thickness, h (inch): 6.25
 State: Uncracked
 Compressive strength, f_c (psi): 2500
 Ψ_{cv} : 1.4
 Reinforcement condition: B tension, B shear
 Supplemental reinforcement: No
 Reinforcement provided at corners: No
 Ignore concrete breakout in tension: No
 Ignore concrete breakout in shear: No
 Ignore s_{do} requirement: Not applicable
 Build-up grout pad: No

Base Plate
 Length x Width x Thickness (inch): 3.15 x 50.00 x 0.25

Recommended Anchor
 Anchor Name: Titen HD® Flat Washer Head - 1/2"Ø Titen HD Flat Washer, hnom: 4" (102mm)
 Code Report: ICC-ES ESR-2713



Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.
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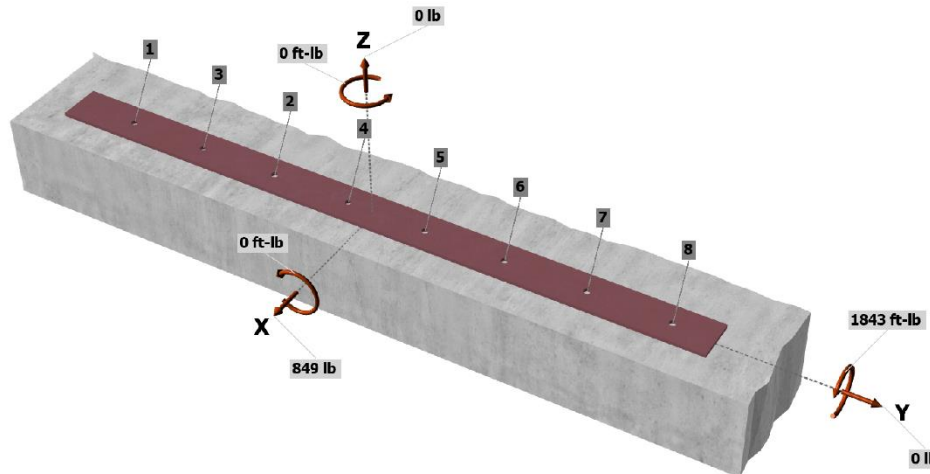


Company:		Date:	6/8/2022
Engineer:		Page:	2/6
Project:			
Address:			
Phone:			
E-mail:			

Load and Geometry
 Load factor source: ACI 318 Section 5.3
 Load combination: $U = 1.2D + 1.0W + 1.0L + 0.5(Lr \text{ or } S \text{ or } R)$
 Seismic design: No
 Anchors subjected to sustained tension: Not applicable
 Apply entire shear load at front row: No
 Anchors only resisting wind and/or seismic loads: No

Service level loads:	D	W	L	Lr/S/R	Strength level loads
N_x [lb]:	0	0	0	0	0
V_{ax} [lb]:	0	649	200	0	849
V_{ay} [lb]:	0	0	0	0	0
M_x [ft-lb]:	0	0	0	0	0
M_y [ft-lb]:	0	1193	650	0	1843
M_z [ft-lb]:	0	0	0	0	0

<Figure 1>



Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.
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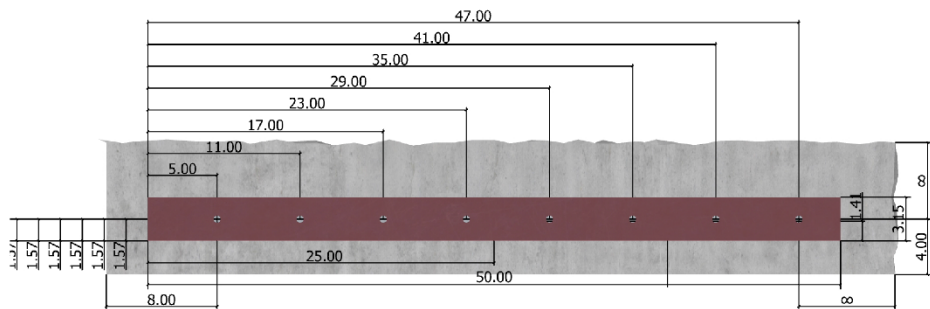
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Strong-Tie Software
 Version 3.0.7947.8

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Phone:			
E-mail:			

<Figure 2>



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Phone:			
E-mail:			

3. Resulting Anchor Forces

Anchor	Tension load, N _{ua} (lb)	Shear load x, V _{uxx} (lb)	Shear load y, V _{uyy} (lb)	Shear load combined, √(V _{uxx}) ² +√(V _{uyy}) ² (lb)
1	2143.5	117.9	0.0	117.9
2	2100.7	111.2	0.0	111.2
3	2118.6	114.5	0.0	114.5
4	2082.7	107.8	0.0	107.8
5	2064.8	104.4	0.0	104.4
6	2046.9	101.1	0.0	101.1
7	2028.9	97.7	0.0	97.7
8	2011.0	94.3	0.0	94.3
Sum	16597.1	849.0	0.0	849.0

Maximum concrete compression strain (%): 0.22
 Maximum concrete compression stress (psi): 970
 Resultant tension force (lb): 16597
 Resultant compression force (lb): 16597
 Eccentricity of resultant tension forces in x-axis, e'_{tx} (inch): 0.28
 Eccentricity of resultant tension forces in y-axis, e'_{ty} (inch): 0.00
 Eccentricity of resultant shear forces in x-axis, e'_{vx} (inch): 0.00
 Eccentricity of resultant shear forces in y-axis, e'_{vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

N _{sa} (lb)	φ	φN _{sa} (lb)
20130	0.65	13085

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5}$ (Eq. 17.4.2.2a)

k _c	λ _a	f _c (psi)	h _{ef} (in)	N _b (lb)
24.0	1.00	2500	2.990	6204

$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. 17.3.1 & Eq. 17.4.2.1b)

A _{Nc} (in ²)	A _{Nco} (in ²)	c _{a,min} (in)	Ψ _{ec,N}	Ψ _{ed,N}	Ψ _{c,N}	Ψ _{cp,N}	N _b (lb)	φ	φN _{cbg} (lb)
432.51	80.46	4.00	0.941	0.968	1.00	0.997	6204	0.65	19671

8. Steel Strength of Anchor in Shear (Sec. 17.5.1)

V _{sa} (lb)	φ _{grout}	φ	φ _{grout} φV _{sa} (lb)
7455	1.0	0.60	4473

9. Concrete Breakout Strength of Anchor in Shear (Sec. 17.5.2)

Shear perpendicular to edge in x-direction:

$V_{bx} = \min[7(f_e / d_s)^{0.2} \lambda_a \sqrt{f_c} c_{s1}^{1.5}; 9 \lambda_a \sqrt{f_c} c_{s1}^{1.5}]$ (Eq. 17.5.2.2a & Eq. 17.5.2.2b)

f _e (in)	d _s (in)	λ _a	f _c (psi)	c _{s1} (in)	V _{bx} (lb)
2.99	0.500	1.00	2500	4.00	2834

$\phi V_{cbx} = \phi (A_{Vc} / A_{Vco}) \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_{bx}$ (Sec. 17.3.1 & Eq. 17.5.2.1a)

A _{Vc} (in ²)	A _{Vco} (in ²)	Ψ _{ed,V}	Ψ _{c,V}	Ψ _{h,V}	V _{bx} (lb)	φ	φV _{cbx} (lb)

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E-mail:			

72.10	72.10	1.000	1.400	1.000	2834	0.70	2778
-------	-------	-------	-------	-------	------	------	------

Shear perpendicular to edge in y-direction:

$V_{by} = \min\{7(l_e/d_a)^{0.2}\sqrt{d_a\lambda_a\sqrt{f_c}C_{st}^{1.5}}; 9\lambda_a\sqrt{f_c}C_{st}^{1.5}\}$ (Eq. 17.5.2.2a & Eq. 17.5.2.2b)

l_e (in)	d_a (in)	λ_a	f_c (psi)	C_{st} (in)	V_{by} (lb)
2.99	0.500	1.00	2500	8.00	8008

$\phi V_{cbx} = \phi (A_{vc}/A_{vco})\psi_{ed,v}\psi_{c,v}\psi_{h,v}V_{by}$ (Sec. 17.3.1 & Eq. 17.5.2.1a)

A_{vc} (in ²)	A_{vco} (in ²)	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{by} (lb)	ϕ	ϕV_{cbx} (lb)
100.02	288.00	0.800	1.400	1.386	8008	0.70	3021

Shear parallel to edge in x-direction:

$V_{bx} = \min\{7(l_e/d_a)^{0.2}\sqrt{d_a\lambda_a\sqrt{f_c}C_{st}^{1.5}}; 9\lambda_a\sqrt{f_c}C_{st}^{1.5}\}$ (Eq. 17.5.2.2a & Eq. 17.5.2.2b)

l_e (in)	d_a (in)	λ_a	f_c (psi)	C_{st} (in)	V_{bx} (lb)
2.99	0.500	1.00	2500	4.00	2834

$\phi V_{cbx} = \phi (2)(A_{vc}/A_{vco})\psi_{ed,v}\psi_{c,v}\psi_{h,v}V_{bx}$ (Sec. 17.3.1, 17.5.2.1(c) & Eq. 17.5.2.1b)

A_{vc} (in ²)	A_{vco} (in ²)	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)	
72.10	72.10	1.000	1.000	1.400	1.000	2834	0.70	5555

Shear parallel to edge in y-direction:

$V_{by} = \min\{7(l_e/d_a)^{0.2}\sqrt{d_a\lambda_a\sqrt{f_c}C_{st}^{1.5}}; 9\lambda_a\sqrt{f_c}C_{st}^{1.5}\}$ (Eq. 17.5.2.2a & Eq. 17.5.2.2b)

l_e (in)	d_a (in)	λ_a	f_c (psi)	C_{st} (in)	V_{bx} (lb)
2.99	0.500	1.00	2500	44.00	103293

$\phi V_{cbx} = \phi (2)(A_{vc}/A_{vco})\psi_{ed,v}\psi_{c,v}\psi_{h,v}V_{bx}$ (Sec. 17.3.1, 17.5.2.1(c) & Eq. 17.5.2.1a)

A_{vc} (in ²)	A_{vco} (in ²)	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{bx} (lb)	ϕ	ϕV_{cbx} (lb)
437.50	8712.00	1.000	1.400	3.250	103293	0.70	33039

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.5.3)

$\phi V_{cp} = \phi k_{cp}N_{cb} = \phi k_{cp}(A_{Nc}/A_{Nco})\psi_{ed,N}\psi_{c,N}\psi_{cp,N}N_b$ (Sec. 17.3.1 & Eq. 17.5.3.1a)

k_{cp}	A_{Nc} (in ²)	A_{Nco} (in ²)	$\psi_{ed,N}$	$\psi_{c,N}$	$\psi_{cp,N}$	N_b (lb)	ϕ	ϕV_{cp} (lb)
2.0	50.91	80.46	0.968	1.000	0.997	6204	0.70	5300

11. Results

Interaction of Tensile and Shear Forces (Sec. R17.6)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	2143	13085	0.16	Pass
Concrete breakout	16597	19671	0.84	Pass (Governs)

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	118	4473	0.03	Pass
T Concrete breakout x+	849	2778	0.31	Pass
T Concrete breakout y-	0	3021	0.00	Pass
Concrete breakout x+	0	5555	0.00	Pass
Concrete breakout y-	755	33039	0.02	Pass
Concrete breakout, combined	-	-	0.31	Pass (Governs)
Pryout	115	5300	0.02	Pass

Interaction check	$(N_{ua}/\phi N_n)^{5/3}$	$(V_{ua}/\phi V_n)^{5/3}$	Combined Ratio	Permissible	Status

Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.
 Simpson Strong-Tie Company Inc. 5956 W. Las Positas Boulevard Pleasanton, CA 94588 Phone: 925.560.9000 Fax: 925.847.3871 www.strongtie.com

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
		Project #: EEV-22-0712	
	Engineer: LL	PER: 8127	Page #: Page 56 of 60



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Company:		Date:	6/8/2022
Engineer:		Page:	6/6
Project:			
Address:			
Phone:			
E-mail:			

Sec. R17.6 0.75 0.14 89.2% 1.0 Pass

1/2"Ø Titen HD Flat Washer, hnom:4" (102mm) meets the selected design criteria.

12. Warnings

- For irregular anchor patterns, the designer must consider sizing of base plate holes to ensure shear loads are distributed to anchors as designed.
- Designer must exercise own judgement to determine if this design is suitable.
- Refer to manufacturer's product literature for hole cleaning and installation instructions.


Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.
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DEWALT	DEWALT DESIGN ASSIST 1.6.3.0	Page 1
	BR80 Supplemental Anchor Calculation	Jul 21 2022
1. Project Information		
Company: Project Engineer: -- Address: -- Florida 33004 Phone: M: - P: - Email: llopes@buildingdrops.com Project Name: Untitled Project Address: Untitled Notes:		
2. Selected Anchor Information		
Selected Anchor : Screw-Bolt+ (Flat Head) Brand: DEWALT Material: 1/2" Ø Low Carbon Steel Embedment, h_{nom}: h _{ef} 1.75 in h _{nom} 2.5 in Approval: ICC-ES ESR-3889 Issued/Revision: Nov,2021 - Drill method: Hammer Drilled		
		
3. Design Principles		
Design Method: ACI 318-14 Load Combinations: Section 5.3 $U = 1.2 (D) + (W) + (L) + 0.5 (L_r)$		
4. Base Material Information		
Concrete: Type: Uncracked Normal Weight Concrete Strength: 3625 psi Reinforcement: Supplemental Reinforcement: False Spacing: Tension No (Condition B) Shear No (Condition B) Controls Breakout: Tension False Shear False Base Plate: Sizing: Thickness 0.25 in Length 3.15 in Width 50 in Standoff: None Height 0 in Strength: 36000 psi Profile: None		
Input data and results must be checked for agreement with the existing conditions, the standards and guidelines and must be checked for plausibility		

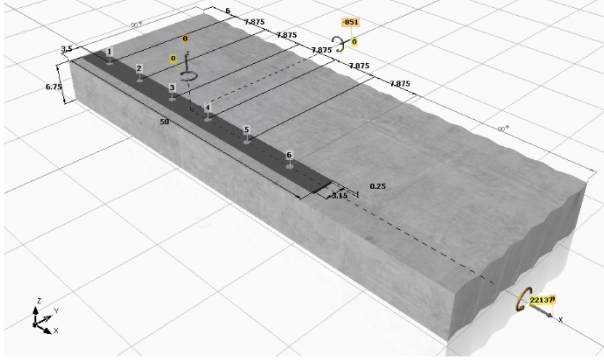
Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
		Project #: EEV-22-0712	
	Engineer: LL	PER: 8127	Page #: Page 58 of 60



DEWALT DESIGN ASSIST 1.6.3.0 Page 2

BR80 Supplemental Anchor Calculation Jul 21 2022

5. Geometric Conditions



h_{slab}	6.75	in	h_{min}	4.000	in
Edge Cx-	6	in	c_{min}	1.750	in
Edge Cx+	∞	in	c_{ac}	3.300	in
Edge Cy-	3.5	in	s_{min}	2.750	in
Edge Cy+	∞	in			

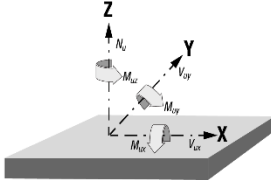
6. Summary Results

Tension Loading					
Design Proof	Demand(lb)	Capacity(lb)	Utilization	Status	Critical
Steel Strength:	2661.00	13309.00	0.200	OK	
Concrete Breakout Strength:	15868.00	15957.00	0.994	OK	Controls

Shear Loading					
Design Proof	Demand(lb)	Capacity(lb)	Utilization	Status	Critical
Steel Strength	147.00	5316.00	0.028	OK	
Concrete Breakout Strength:	851.00	11014.00	0.077	OK	Controls
Pryout Strength	851.00	17562.00	0.048	OK	

Input data and results must be checked for agreement with the existing conditions, the standards and guidelines and must be checked for plausibility

Project Description: Hardware And Glass Shoe and Anchor Options	Date: August 3, 2022	Customer: Hardware and Glass Group LLC	
		Project #: EEV-22-0712	
	Engineer: LL	PER: 8127	Page #: Page 59 of 60

DEWALT	DEWALT DESIGN ASSIST 1.6.3.0	Page 3			
	BR80 Supplemental Anchor Calculation	Jul 21 2022			
7. Warnings and Remarks					
ANCHOR DESIGN CRITERIA IS SATISFIED ✔					
<ul style="list-style-type: none"> The results of the calculations carried out by means of the DDA Software are based essentially on the data you put in. Therefore, you bear the sole responsibility for the absence of errors, the completeness and the relevance of the data to be put in by you. Moreover, you bear sole responsibility for having the results of the calculation checked and cleared by an design professional/engineer, particularly with regard to compliance with applicable standards, norms and permits, prior to using them for your specific project. The DDA Software serves only as an aid to interpret standards, norms and permits without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application. 					
8. Load Condition					
Design Loads / Actions					
Nu	0 lb	Vux	0 lb	Vuy	-851 lb
Muz	0 in-lb	Mux	22137 in-lb	Muy	0 in-lb
Consider Load Reversal		X Direction	0%	Y Direction	0%
					
Input data and results must be checked for agreement with the existing conditions, the standards and guidelines and must be checked for plausibility					

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		Project #: EEV-22-0712	
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